

# GEOTECHNICAL AND GEOLOGIC HAZARDS INVESTIGATION HILLSIDE DRIVE IMPROVEMENTS DELTA, COLORADO PROJECT#01123-0006

CITY OF DELTA 640 W. 4<sup>TH</sup> STREET DELTA, COLORADO 81416

**JANUARY 24, 2023** 

Huddleston-Berry Engineering and Testing, LLC 2789 Riverside Parkway Grand Junction, Colorado 81501

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# **1.0 INTRODUCTION**

As part of continued infrastructure improvements, the City of Delta proposes to reconstruct Hillside Drive between approximately E. 4<sup>th</sup> Street and E. 6<sup>th</sup> Street. As part of the design development process, Huddleston-Berry Engineering and Testing, LLC (HBET) was retained by the City of Delta to conduct a geologic hazards and geotechnical investigation at the site.

#### 1.1 Scope

As discussed above, a geologic hazards and geotechnical investigation was conducted for Hillside Drive improvements project in Delta, Colorado. The scope of the investigation included the following components:

- Conducting a subsurface investigation to evaluate the subsurface conditions at the site.
- Collecting soil samples and conducting laboratory testing to determine the engineering properties of the soils at the site.
- Providing recommendations for excavations, subgrade preparation, and pavements.
- Evaluating potential geologic hazards at the site.

The investigation and report were completed by a Colorado registered professional engineer in accordance with generally accepted geotechnical and geological engineering practices. This report has been prepared for the exclusive use of the City of Delta.

#### **1.2** Site Location and Description

The site includes Hillside Drive, between approximately E.  $4^{\text{th}}$  Street and E.  $6^{\text{th}}$  Street, in Delta, Colorado. The project location is shown on Figure 1 – Site Location Map.

At the time of the investigation, Hillside Drive consisted of one lane in each direction. The area included primarily residential properties. The general slope of the roadway was moderately down to the north.

## 2.0 GEOLOGIC SETTING

#### 2.1 Soils

Soils data was obtained from the USDA Natural Resource Conservation Service Web Soil Survey. The data indicates that the site is underlain by Urban land. Soil survey data is included in Appendix A.



### 2.2 Geology

According to the *Geologic Map of the Delta Quadrangle, Delta and Montrose Counties, Colorado* (2008), most of Hillside Drive lies on landslide deposits. Alluvial deposits of the Uncompany River are mapped at the higher elevations east of Hillside Drive and at the lower elevations west of Hillside Drive.

### 2.3 Groundwater

Groundwater was only encountered in B-1 at a depth of 10.0 feet and in B-4 at a depth of 5.0 feet at the time of the investigation. However, based upon the soil types encountered and location of B-4 on the hillside, the shallow groundwater in B-4 is likely perched and not representative of a static groundwater elevation.

## **3.0 FIELD INVESTIGATION**

#### 3.1 Subsurface Investigation

The subsurface investigation was conducted on November  $14^{th}$ , 2019 and consisted of five geotechnical borings. The borings were drilled to depths of between 6.0 and 15.0 feet below the existing ground surface. Boring locations are shown on Figure 2 – Site Plan. Typed boring logs are included in Appendix B. Samples of the native soils were collected during Standard Penetration Testing (SPT) and using bulk sampling methods at the locations shown on the logs.

As shown on the logs, the subsurface conditions were variable. Boring B-1, conducted at the lower elevation at the north end of the project area, encountered 4-inches of asphalt pavement above granular base course to a depth of approximately 2.0 feet. Below the base course, brown, moist to wet, medium stiff to stiff sandy lean clay to lean clay with sand extended to a depth of 12.5 feet. The clay was underlain by brown, wet, dense sandy gravel and cobbles to the bottom of the boring. Groundwater was encountered in B-1 at a depth of 10.0 feet at the time of the investigation.

Borings B-2 and B-4, conducted along Hillside Drive as it climbed the hill, encountered 4 to 5-inches of asphalt pavement. In B-4, granular base course extended to a depth of approximately 3.0 feet. Below the asphalt in B-2 and below the base course in B-4, black to brown, loose to medium dense silty gravel with sand was encountered. The gravel extended to the bottom of B-2. In B-4, the gravel extended to a depth of 12.5 feet where shale bedrock was encountered. Groundwater was not encountered in B-2 but was encountered in B-4 at a depth of 5.0 feet at the time of the investigation.

Borings B-3 and B-5, conducted at the higher elevations in the southern and eastern portions of the site, encountered 4-inches of asphalt pavement. In B-5, granular base course extended to a depth of approximately 2.0 feet. Below the asphalt in B-3 and below the base course in B-5, tan, moist, dense to very dense sandy gravel and cobbles extended to the bottoms of the borings where auger refusal was encountered. Groundwater was not encountered in B-3 or B-5 at the time of the investigation.



# 4.0 LABORATORY TESTING

Selected native soil and bedrock samples collected from the borings were tested in the Huddleston-Berry Engineering and Testing LLC geotechnical laboratory for natural moisture content, grain size analysis, and Atterberg limits. The laboratory testing results are included in Appendix C.

The laboratory testing results indicate that the native clay soils are slightly to moderately plastic. In general, based upon the plasticity of the material, the native clay soils may have a slight potential for expansion.

The native silty gravel soils were indicated to be very slightly plastic. Based upon our experience with similar soils, the native silty gravel soils are anticipated to be slightly collapsible.

The shale bedrock at the site was indicated to be moderately plastic. Based upon the Atterberg limits of the material and upon our experience with the Mancos shale in Western Colorado, the shale bedrock at this site is anticipated to be slightly expansive.

## 5.0 GEOLOGIC INTERPRETATION

### 5.1 Geologic Hazards

As indicated previously, most of the roadway is mapped as being underlain by landslide deposits. Although no evidence of active movements was observed at the time of the investigation, shallow groundwater was encountered in B-4 and it is important to note that most mass earth movements are associated with excess moisture. As discussed previously, the observed groundwater at this location is likely perched. However, given that groundwater was not encountered in B-2, B-3, or B-5, the presence of shallow groundwater in B-4 raises some concerns regarding the long-term stability of the hillside.

In addition to the shallow groundwater in the hillside, moisture sensitive soils and bedrock are also present at the site.

#### 5.2 Geologic Constraints

In general, the primary geologic constraint to construction at the site is the fact that most of the roadway is underlain by landslide deposits.

#### 5.3 Water Resources

No water supply wells were observed in the project area. As discussed previously, shallow groundwater was encountered in some areas of the site. In general, with proper design and construction, the proposed construction is not anticipated to adversely impact surface water or groundwater.



#### 5.4 Mineral Resources

Potential mineral resources in western Colorado generally include gravel, uranium ore, and commercial rock products such as flagstone. As discussed previously, portions of the site are mapped as being underlain by gravels. In addition, gravels were encountered in the subsurface at the site. However, based upon the current land use at the site and surrounding properties, HBET does not believe that the gravels represent an economically recoverable resource.

## 6.0 CONCLUSIONS

Based upon the available data sources, field investigation, and nature of the proposed construction, HBET does not believe that there are any geologic conditions which should preclude construction at this site. However, pavements, utility installation, and/or earthwork may have to consider the impacts of moisture sensitive soils and/or bedrock. In addition, the presence of groundwater in B-4 raises concerns regarding the long-term stability of the hillside.

## 7.0 **RECOMMENDATIONS**

### 7.1 Corrosion of Concrete

Water soluble sulfates are common to the soils and bedrock in Western Colorado. Therefore, at a minimum, Type I-II sulfate resistant cement is recommended for this site.

#### 7.2 Lateral Earth Pressures

Any retaining walls should be designed to resist lateral earth pressures. For backfill consisting of the native soils or imported granular, non-free draining, non-expansive material, we recommend that the walls be designed for an active equivalent fluid unit weight of 55 pcf in areas where no surcharge loads are present. Passive pressure should be ignored. Lateral earth pressures should be increased as necessary to reflect any surcharge loading behind the walls.

#### 7.3 Excavations

Excavations in the soils at the site may stand for short periods of time but should not be considered to be stable. In general, the site soils classify as Type C soil with regard to OSHA's Construction Standards for Excavations. For Type C soils, the maximum allowable slope in temporary cuts is 1.5H:1V. Subgrade Preparation.



### 7.4 Pavements

The proposed construction is anticipated to include new pavements along Hillside Drive and the new pavements may extend into portions of the intersecting streets. As discussed previously, the native pavement subgrade materials at the site range from clay soils to gravel and cobble soils. Where clays are present in the subgrade, HBET recommends the minimum Resilient Modulus of 3,000 psi be used. Where gravel and cobble soils are present in the subgrade, a Resilient Modulus of 4,500 psf may be used.

Traffic date provided to HBET suggest that the Average Daily Traffic (ADT) at the end of 2022 was approximately 3,500 vehicles. This corresponds to an estimated ESAL value of approximately 665,000 as indicated on the ESAL calculations included in Appendix D. Based upon the traffic loading and subgrade conditions, the following pavement section alternatives are recommended:

#### Clay Soils in Subgrade

ESAL's = 665,000;	Structural Number =	= 4.10
~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		

	PAVEMENT SECTION (Inches)										
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL						
А	4.0	18.0			22.0						
В	5.0	14.0			19.0						
С	4.0	6.0	16.0		30.0						
Rigid Pavement		6.0		8.0	14.0						

Gravel Soils in Subgrade

ESAL's = 665,000;	Structural Number = 3.7
~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	

	PAVEMENT SECTION (Inches)										
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL						
А	4.0	15.0			19.0						
В	5.0	12.0			17.0						
С	4.0	6.0	12.0		22.0						
Rigid Pavement		6.0		8.0	14.0						

The pavement section alternatives below can be reduced by incorporating a geogrid such as Haynes RX1100, Tensar TX5, Mirafi BXG110, or equivalent into the section. The geogrid reinforced alternatives are:

## Clay Soils in Subgrade

	PAVEMENT SECTION (Inches)										
ALTERNATIVE	Hot-Mix Asphalt	CDOT Class 6	Geogrid	TOTAL							
	Favement	Dase Course	Location	IUIAL							
А	4.0	11.0	Below base	15.0							
В	5.0	8.0	Below base	13.0							



<u>Gravel Soils in Subgrade</u>

	PAVEMENT SECTION (Inches)									
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	Geogrid Location	TOTAL						
А	4.0	8.0	Below base	12.0						
В	5.0	6.0	Below base	11.0						

Prior to new pavement placement, areas to be paved should be stripped of all topsoil, uncontrolled fill, or other unsuitable materials. It is recommended that the subgrade soils be scarified to a depth of 12-inches; moisture conditioned, and recompacted to a minimum of 95% of the standard Proctor maximum dry density, within  $\pm 2\%$  of optimum moisture content as determined by AASHTO T-99.

Aggregate base course and subbase course should be placed in maximum 9-inch loose lifts, moisture conditioned, and compacted to a minimum of 95% and 93% of the maximum dry density, respectively, at -2% to +3% of optimum moisture content as determined by AASHTO T-180. In addition to density testing, base course should be proofrolled to verify subgrade stability.

It is recommended that Hot-Mix Asphaltic (HMA) pavement conform to CDOT grading SX or S specifications and consist of an approved 75 gyration Superpave method mix design. HMA pavement should be compacted to between 92% and 96% of the maximum theoretical density. An end point stress of 50 psi should be used. It is recommended that rigid pavements consist of CDOT Class P concrete or alternative approved by the Engineer. In addition, pavements should conform to local specifications.

The long-term performance of the pavements is dependent on positive drainage away from the pavements. Ditches, culverts, and inlet structures in the vicinity of paved areas must be maintained to prevent ponding of water on the pavement.

#### 7.5 Additional Investigation

As discussed previously, shallow groundwater was encountered in B-4 which was conducted on the hillside and this raises concerns regarding the long-term stability of the hillside. In order to further evaluate the water at this location, HBET recommends that additional investigation be conducted during the construction. Specifically, HBET recommends that test pits be excavated in the vicinity of B-4 to determine the precise nature and extent of the water and to evaluate whether or not additional drainage measures are necessary to mitigate the water.

## 8.0 GENERAL

The recommendations included above are based upon the results of the subsurface investigation and on our local experience. These conclusions and recommendations are valid only for the proposed construction.



As discussed previously, the subsurface conditions at the site were variable. However, the precise nature and extent of any subsurface variability may not become evident until construction. Therefore, it is recommended that a representative of HBET observe the foundation excavations prior to structural fill placement to verify that the subsurface conditions are consistent with those described herein. In addition, it is recommended that a representative of HBET test compaction of structural fill materials.

As discussed previously, moisture sensitive soils and bedrock were encountered at the site. The recommendations contained herein are designed to reduce the potential for excessive differential movements; however, HBET cannot predict long-term changes in subsurface moisture conditions and/or the precise magnitude or extent of volume change. *Where significant increases in subsurface moisture occur due to poor grading, improper stormwater management, utility line failure, excess irrigation, or other cause, significant movements, including slope failures along the hillside, are possible.* 

Huddleston-Berry Engineering and Testing, LLC is pleased to be of service to your project. Please contact us if you have any questions or comments regarding the contents of this report.

Respectfully Submitted: Huddleston-Berry Engineering and Testing, LLC



Michael A. Berry, P.E. Vice President of Engineering

**FIGURES** 





APPENDIX A Soil Survey Data





**Natural Resources Conservation Service** 

Web Soil Survey National Cooperative Soil Survey





# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
900	Urban land	5.3	100.0%
Totals for Area of Interest		5.3	100.0%



# Map Unit Description

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions in this report, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named, soils that are similar to the named components, and some minor components that differ in use and management from the major soils.

Most of the soils similar to the major components have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Some minor components, however, have properties and behavior characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities. Soils that have profiles that are almost alike make up a *soil series*. All the soils of a series have major horizons that are similar in composition, thickness, and arrangement. Soils of a given series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Additional information about the map units described in this report is available in other soil reports, which give properties of the soils and the limitations, capabilities, and potentials for many uses. Also, the narratives that accompany the soil reports define some of the properties included in the map unit descriptions.

# **Report—Map Unit Description**

# Ridgway Area, Colorado, Parts of Delta, Gunnison, Montrose, and Ouray Counties

900—Urban land

Map Unit Composition Urban land: 100 percent



Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Urban Land**

#### Interpretive groups

Land capability classification (irrigated): 8 Land capability classification (nonirrigated): 8 Hydric soil rating: No

## **Data Source Information**

Soil Survey Area: Ridgway Area, Colorado, Parts of Delta, Gunnison, Montrose, and Ouray Counties Survey Area Data: Version 11, Sep 13, 2019



APPENDIX B Typed Boring Logs

	TENRE	Bullion	Huddleston-Berry Engineering & Testing, LLC 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 070-255-6818					BO	RIN	IG N	IUN	<b>1BE</b> PAGE	<b>R B</b>	<b>8-1</b> 0F 1
	CLIEN	IT AL	Istin Civil Group	PROJEC		Hillsid	de Drive							
	PROJ		UMBER 00302-0050	PROJEC	T LOCAT		Delta, CO							
F	DATE	STAR	TED _11/14/19 COMPLETED _11/14/19 (	GROUND ELEVATION HOLE SIZE _4-inches										
	DRILL	ING C	ONTRACTOR S. McKracken	GROUND WATER LEVELS:										
	DRILL	ING N	IETHOD Simco 2000 Track Rig	$\blacksquare$ AT TIME OF DRILLING 10.0 ft										
	LOGO	ED B	CM CHECKED BY MAB	<b>▼</b> AT	END OF	DRILL	.ING _10.0	ft						
	NOTE	s		AFTER DRILLING										
	0. DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID LIMIT	PLASTIC PLASTIC LIMIT		FINES CONTENT (%)
	· -		ASPHALTGranular Base Course	~ -										
	2.5		Sandy Lean CLAY (CL) to Lean CLAY with Sand (CL), brow moist to wet, medium stiff to stiff *** Lab Classified SS1	<i>ı</i> n,	ss 1	94	3-4-3 (7)	-		23	38	19	19	67
	5.0													
	7.5		*** Lab Classified SS2		ss 2	100	7-6-5 (11)	_		22	28	16	12	74
			¥											
	- 12.5		Sandy GRAVEL and COBBLES (gw), brown, wet, dense											
	· -				V ss	53	24-23	-						
	15.0	•	Bottom of hole at 15.0 feet.		3		27-20	_						

TESTING.		Huddleston-Berry Engineering & Testing, LLC 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255-6818					BO	RIN	IG N	NUN	1 <b>BE</b> PAGE	<b>R B</b> ≣ 1 0	<b>8-2</b> DF 1
CLIE	ENT Au	stin Civil Group	PROJEC	T NAME	Hillsi	de Drive							
PRO	JECT N	UMBER _00302-0050	PROJECT LOCATION Delta, CO										
DAT	E STAR	TED _11/14/19         COMPLETED _11/14/19	GROUND ELEVATION HOLE SIZE _4-inches										
DRIL	LING C	ONTRACTOR S. McKracken	GROUNE	WATER		LS:							
DRIL	LING N	ETHOD Simco 2000 Track Rig	AT	TIME OF		LING dry							
LOG	GED BI					ING dry							
NOT			АГ				1				FRR	RC	
o DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)				FINES CONTENT (%)
-		ASPHALT Silty GRAVEL with Sand (GM), black to brown, moist, loose medium dense	 e to				_						
<u>2.5</u> - -				SS 1	0	4-4-4 (8)	_						
- 5.0 - - -	<u>الم الم الم الم الم الم الم الم الم الم </u>												
				SS 2	89	7-6-10 (16)	_						
15.0		*** Lab Classified SS3		SS 3	67	14-10-11- 16 (21)			4	19	18	1	20
GEOLECH BH COLU		Bottom of hole at 15.0 feet.											

B	640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970 255 6818					BO	RIN	IG N	NUN	IBE PAGE	<b>R B</b> 1 0	<b>5-3</b> F 1
CLIENT Aus	stin Civil Group	PROJEC		Hillsi	de Drive							
PROJECT NI	JMBER _00302-0050	PROJEC			Delta, CO							
DATE START	TED         11/14/19         COMPLETED         11/14/19	GROUND ELEVATION HOLE SIZE 4-inches										
DRILLING CO	ONTRACTOR S. McKracken	GROUN		R LEVE	LS:							
DRILLING ME	ETHOD Simco 2000 Track Rig	AT	TIME OF	DRIL	LING dry							
LOGGED BY	CM CHECKED BY MAB	AT	END OF	DRILL	ING dry							
NOTES		AF	TER DRI	LLING								
DEPTH (ft) GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT LIMIT			FINES CONTENT (%)
0.0	ASPAHLT										_	-
	*** Auger Rufusal Bottom of hole at 6.0 feet.	very	SS 1	72	20-20-24 (44)							

ESTRACT	BB - CONSUL	Huddleston-Berry Engineering & Testing, LLC 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255-6818					BO	RIN	GN	NUN	<b>IBE</b> PAGE	<b>R B</b>	<b>8-4</b> DF 1
CLIE	NT Au	Istin Civil Group	PROJECT	NAME	Hillsi	de Drive							
PRO		UMBER _00302-0050 F	PROJECT LOCATIONDelta, CO										
DAT	E STAR	TED <u>11/14/19</u> COMPLETED <u>11/14/19</u> C	GROUND ELEVATION HOLE SIZE _4-inches										
DRIL	LING C	ONTRACTOR <u>S. McKracken</u> (											
			⊥ AI ▼ AT			LING 5.0	<u>π</u>						
NOT	GED B						L						
										ATT	FRBF	RG	
0 DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID			FINES CONTEN (%)
- - - 2.5		ASPHALT Granular Base Course											
- - - <u>5.0</u> -		Silty GRAVEL with Sand (gm), brown, moist, loose to mediu dense	um	SS 1	22	5-4-3 (7)	-						
- - - - - -				SS 2	0	4-3-2 (5)	-						
		SHALE, grey, soft to medium hard, highly weathered				10-11-13-	-						
				3	42	20 (24)				46	25	21	
15.0		Bottom of hole at 15.0 feet		V			-						

Esta	B	Huddleston-Berry Engineering & Testing, LLC 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255 6818					BO	RIN	IG N	NUN	<b>IBE</b> PAGE	<b>R E</b> ∃ 1 C	<b>8-5</b> DF 1
CLIE	NT Aus	stin Civil Group	PROJEC	T NAME	Hillsi	de Drive							
PRO.		JMBER _00302-0050	PROJEC	PROJECT LOCATION Delta, CO									
DATE	E START	ED 11/14/19         COMPLETED 11/14/19	GROUN	D ELEVA				HOLE	SIZE	4-inc	hes		
DRIL	LING CO	DNTRACTOR S. McKracken	GROUN		R LEVE	LS:							
DRIL	LING ME	THOD Simco 2000 Track Rig	A1	TIME OF	DRIL	LING dry							
LOG	GED BY	CM CHECKED BY MAB	A1	END OF	DRILL	ING dry							
NOTE	ES		AF	TER DRI	LLING								
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)				FINES CONTENT (%)
0.0		ASPHALT											
		Granular Base Course Sandy GRAVEL and COBBLES (gw), tan, moist, de	nse	SS 1	56	10-13-17 (30)							

APPENDIX C Laboratory Testing Results

	Huddleston-Berry Engineering & Testing, LLC 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255-6818								
	CLIENT Austin Civil Group								PROJECT NAME Hillside Drive
	PROJE		<b>/BER</b> _00	302-0050					PROJECT LOCATION _ Delta, CO
	60 (CL)						CL	СН	
	P L	50							
	A S T I	40							
	C I T Y	30							
	I N D E	20					•	*	
	Х	10							
		0	CL-IVIL	20			40	(ML)	MH     60     80     100
									LIQUID LIMIT
	Sp	ecime	n Identif	ication	LL	PL	PI	#200	Classification
	B-'	1, SS1		11/2019	38	19	19	67	SANDY LEAN CLAY(CL)
	K B-'	1, SS2		11/2019	28	16	12	74	LEAN CLAY with SAND(CL)
ļ	⊾ В-2	2, SS3		11/2019	19	18	1	20	SILTY GRAVEL with SAND(GM)
ŀ	k B-4	4, SS3		11/2019	46	25	21		
18/20									
פחו									
S LAB.									
GP CF3									
GUU-ZU									
200									
PHERG									

APPENDIX D ESAL Calculations



# ESAL CALCULATIONS

Project No.:	00302-0050
Project Name:	Hillside Drive
<b>Client Name:</b>	City of Delta
<b>Completed By:</b>	MAB
Date:	1/18/2023
<b>Current Year:</b>	2023

### GIVEN INFORMATION:

Source: KLJ

Year:	2022	ADT:	3500
Year:		ADT:	

#### **ASSUMPTIONS:**

Growth Rate (%):	2.2
Design Life (yr):	20
Truck Traffic (%):	6
Single Axle (%):	70
Combination (%):	30

#### **DEFINED EQUIVALENCY FACTORS:**

Automobiles Flexible:	0.003
Automobiles Rigid:	0.003
Single Unit Flexible:	0.249
Single Unit Rigid:	0.285
<b>Combination Flexible:</b>	1.087
Combination Rigid:	1.692

#### **CALCULATIONS:**

ADT at Begin	ning	of Design	Life
ADT:	3577	7	

#### ADT at End of Design Life ADT: <u>5528</u>

ADT	at Midp	oint of Design	Life
	ADT:	4552.5	

#### Breakdown of Vehicles Multiplied by Equivalency Factors for Flexible Pavements

Automobiles:	13
Single Unit:	48
Combination:	90

#### Breakdown of Vehicles Multiplied by Equivalency Factors for Rigid Pavement

Automobiles:	13
Single Unit:	55
<b>Combination:</b>	139

Flexible Pavement ESAL's

ESAL's:	661380	

**Rigid Pavement ESAL's** 

**ESAL's:** 906660